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Modern Control for the Secondary Mirror of a Giant Segmented Mirror Telescope

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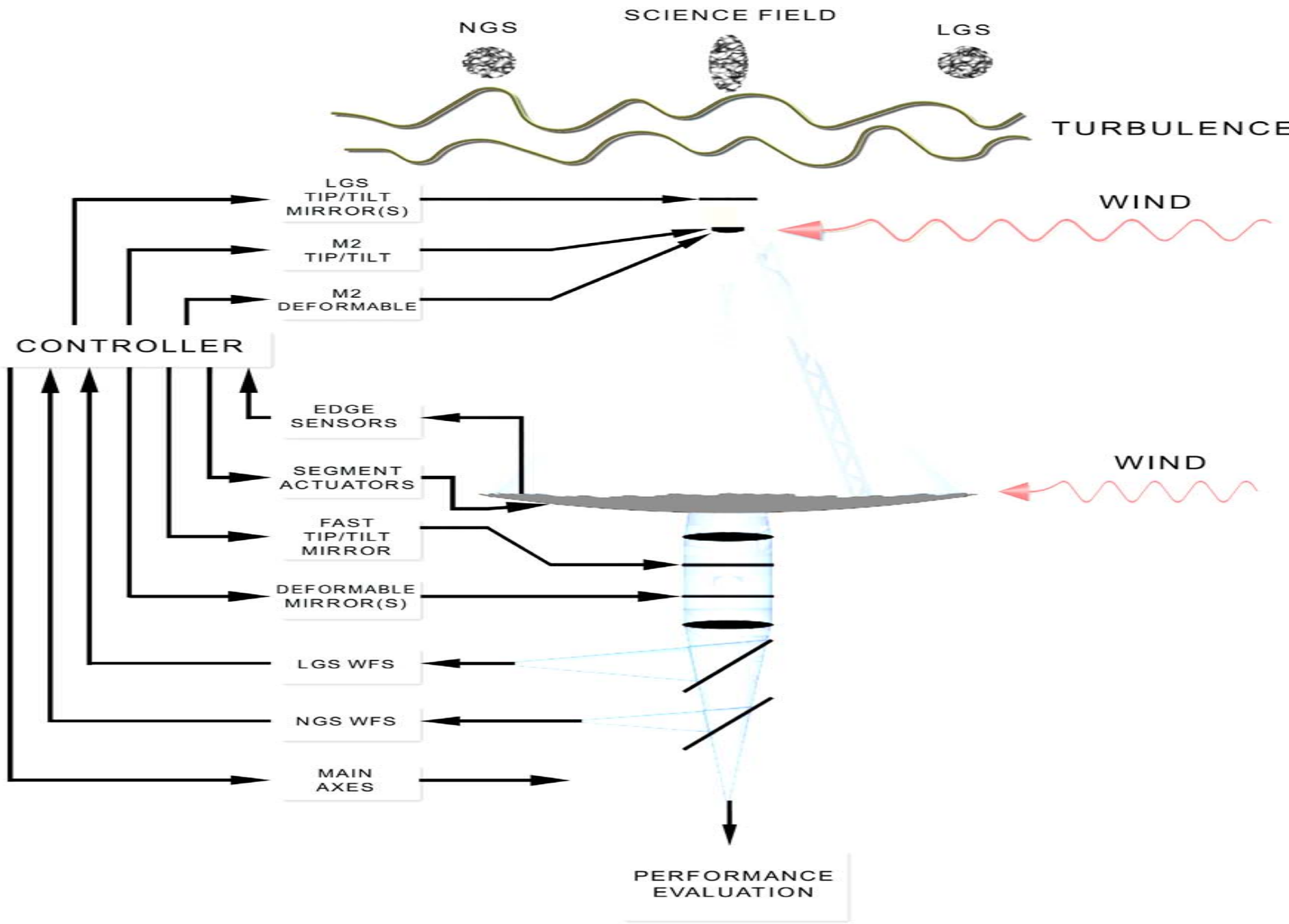


Overview

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- **GSMT Control Philosophy**
- **Modern Control Methods**
- **Secondary Mirror Control Design**
- **Closed Loop Analysis**
- **Conclusions**





Control Philosophy

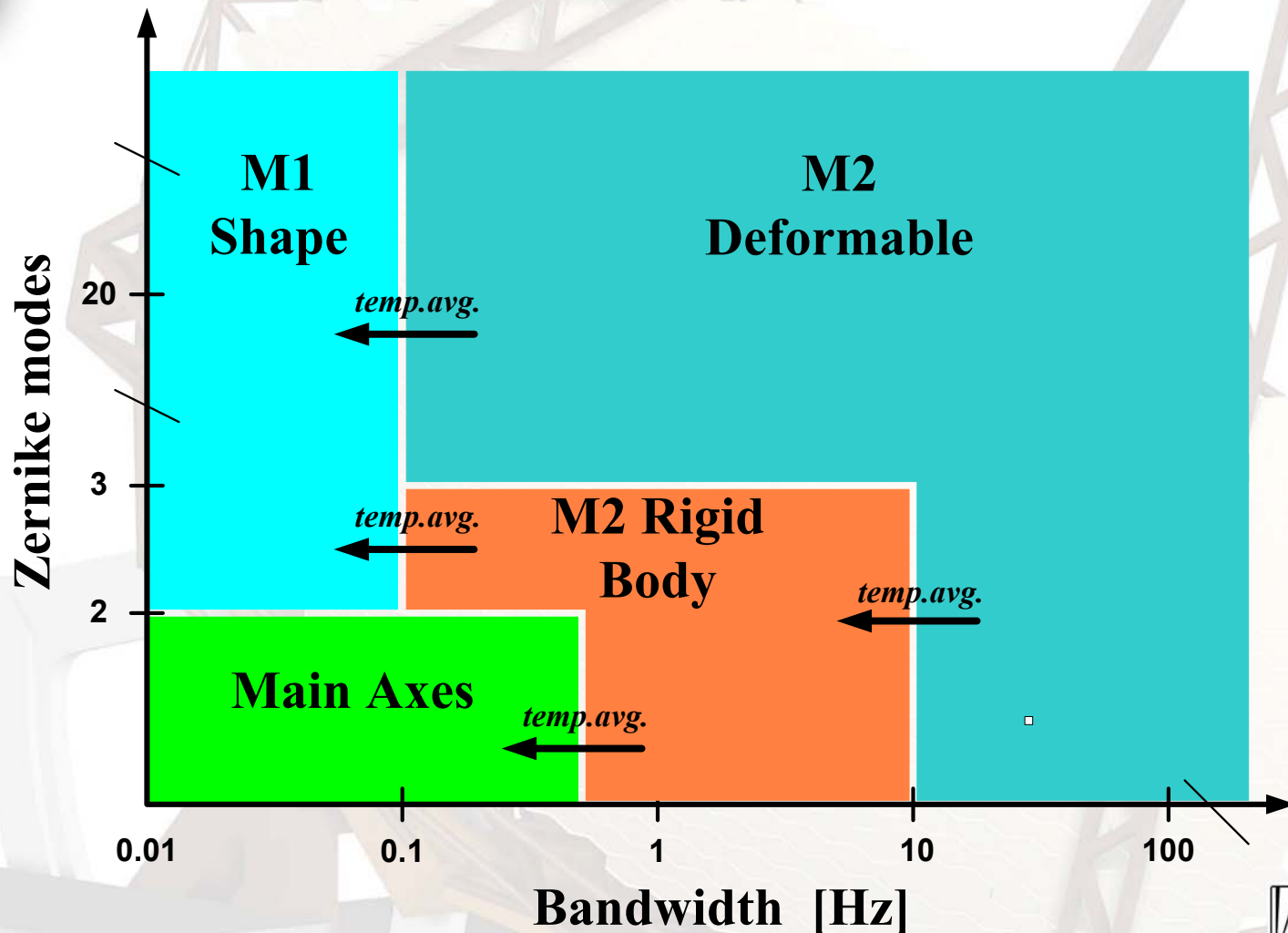
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- **Decentralized Global Control:**
 - Forced decoupling of subsystems
 - Simplifies design and implementation
 - Allows sophisticated control methods where warranted
- **Control Architecture:**
 - Separated in spatial frequency by different sensor/actuator groups
 - Separated in temporal frequency by decoupling control loops from structural dynamics except for one



Frequency separation of subsystems

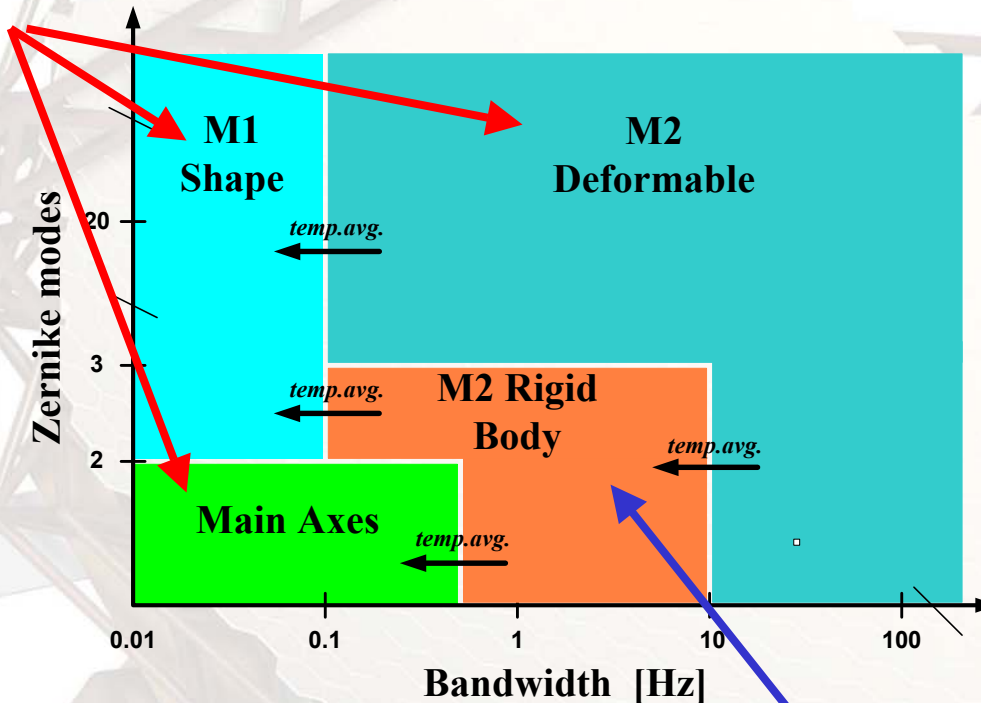
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Frequency separation of subsystems

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Kinematic

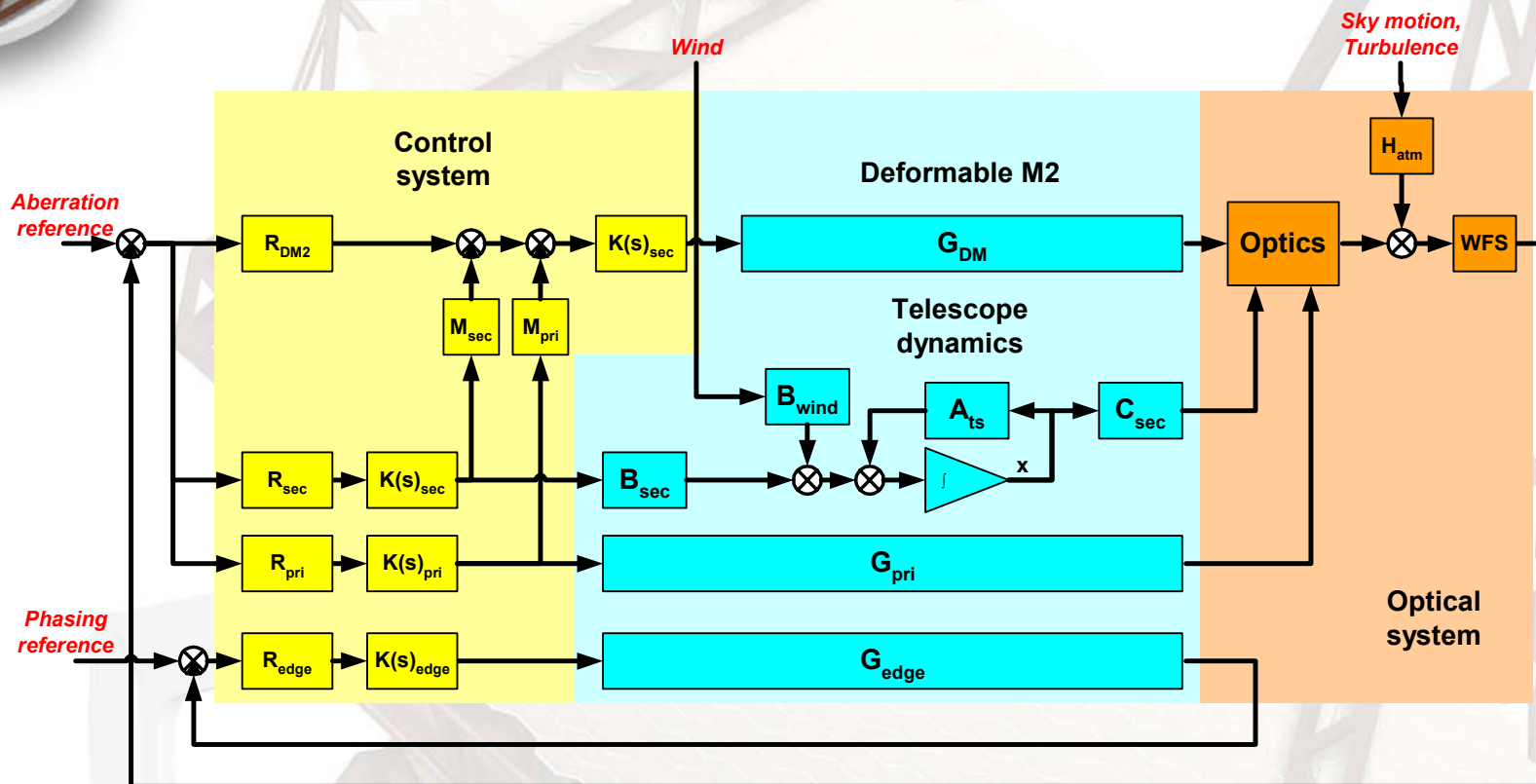


Dynamic



Control configuration

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Objective: demonstrate feasibility of overall control architecture by addressing the M2 dynamic control design



Control Methods

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- **Classical Control:**
 - Single Input/Single Output
 - Well developed / mature theory
 - Does not address multivariable coupling
- **Modern Control:**
 - Multivariable, linear, coupled dynamic systems
 - Distinct set of analysis and design tools
 - Well suited for flexible structures and uncertain dynamic systems



Evolution of Telescope Control

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Telescope systems < 5 m are essentially rigid

⇒ Simple control methods
(*not simple implementation!*)

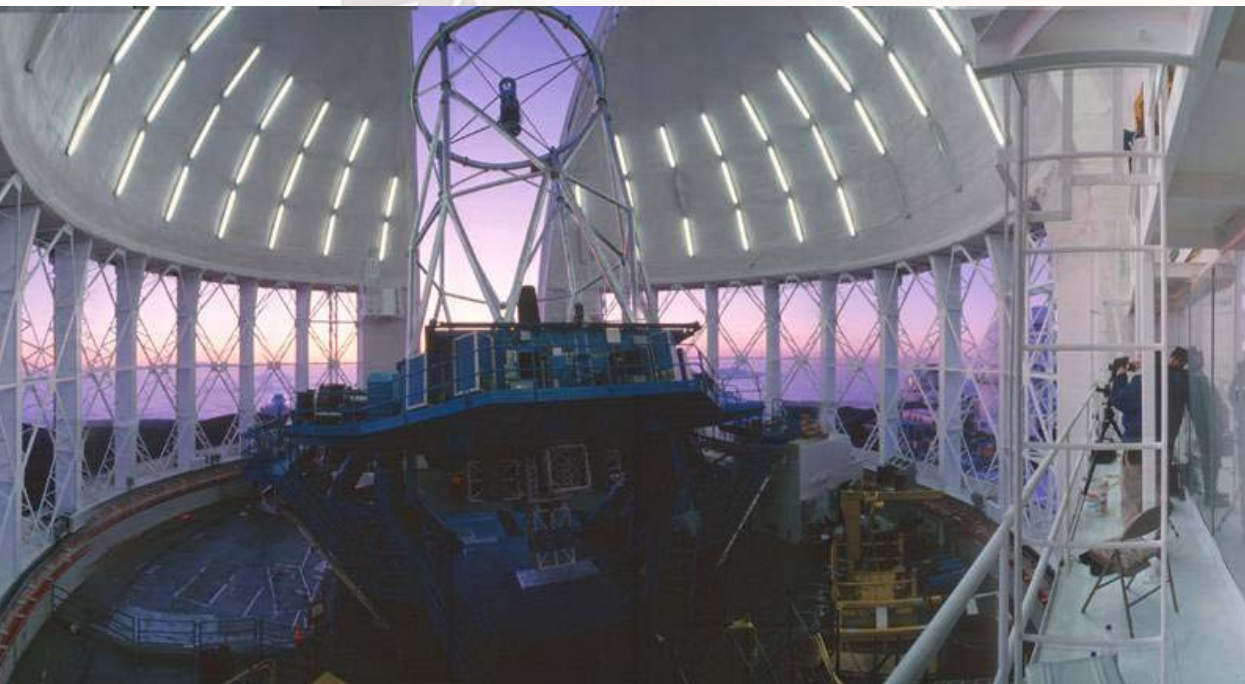


Evolution of Telescope Control

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Telescopes in 5 – 10 m class require controlled optics:

- **Low frequency M1 figure maintenance for deformations**
- **High frequency AO for atmospheric effects**



*Very little interaction
between telescope
structural dynamics
and control systems*

Giant Telescope Control

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- **Giant telescopes require more advanced control technology**
 - **Multivariable coupling between sensor-actuator pairs**
 - **Complex and uncertain structural dynamics**
 - **Greater potential for wind disturbances**
 - **Control / structure interaction**



Giant Telescope CSI

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Lightly damped, clustered low frequency structural modes

Gemini			GSMT		
Mode #	Freq (Hz)	Damping	Mode #	Freq (Hz)	Damping
1	1.82	2.12(%)	1	0.50	2
2	3.24	1.14	2	0.50	2
3	4.13	0.25	3	0.50	2
4	7.08	0.10	4	0.50	2
5	7.74	0.49	5	0.50	2
6	8.88	1.36	6	2.17	2
			7	2.49	2
			8	3.14	2
			9	4.00	2
			10	4.11	2
			11	4.26	2
			12	4.46	2
			13	5.05	2
			14	5.40	2
			15	6.66	2
			16	7.61	2
			17	8.09	2
			18	8.34	2
			19	8.81	2
			20	9.75	2

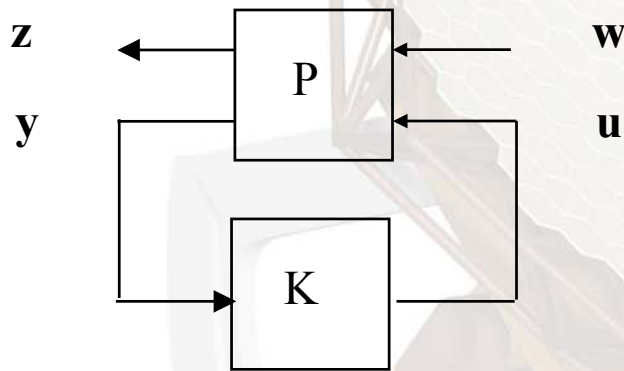
Giant telescope controllers must bridge the gap between M1 figure maintenance and high-frequency AO to compensate for telescope induced aberrations



H₂ Control Methods

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- Good nominal performance
- Performance metric well suited for vibration control
- Potentially poor robustness
- High order controllers



$$K_2 = \arg \left\{ \min_K \|T_{zw}\|_2 \right\}$$

where

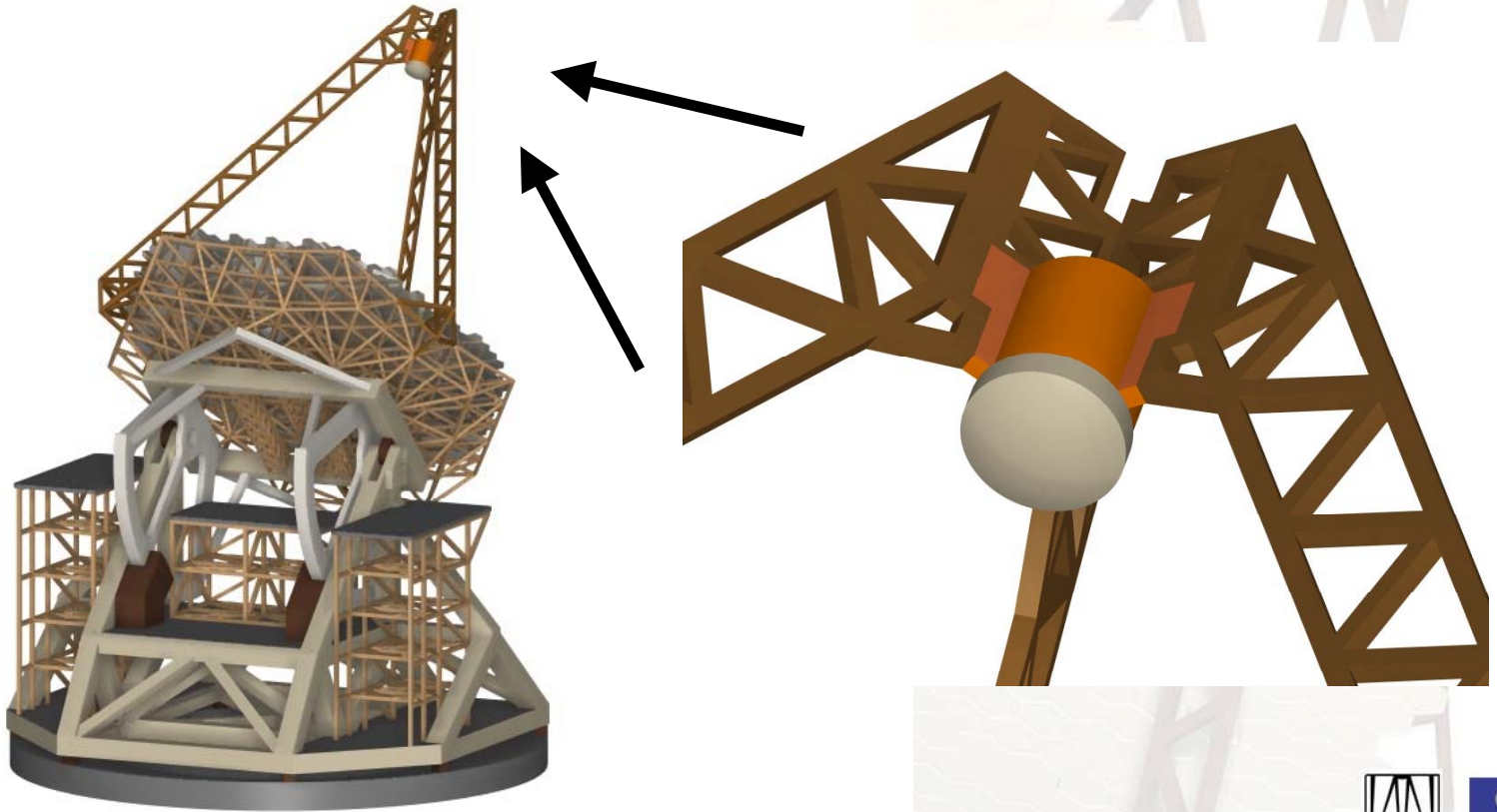
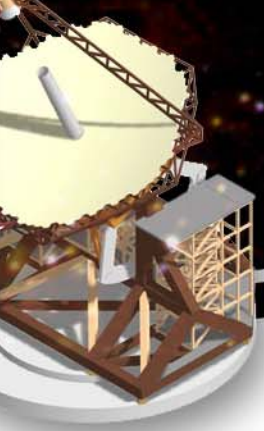
$$\|T_{zw}\|_2 = \lim_{t \rightarrow \infty} E\{z(t)^T z(t)\}$$

$$K_2 : \begin{cases} \dot{x}_c = A_c x_c + B_c y \\ u = C_c x_c \end{cases} \quad x_c \in \mathcal{R}^{nc}$$



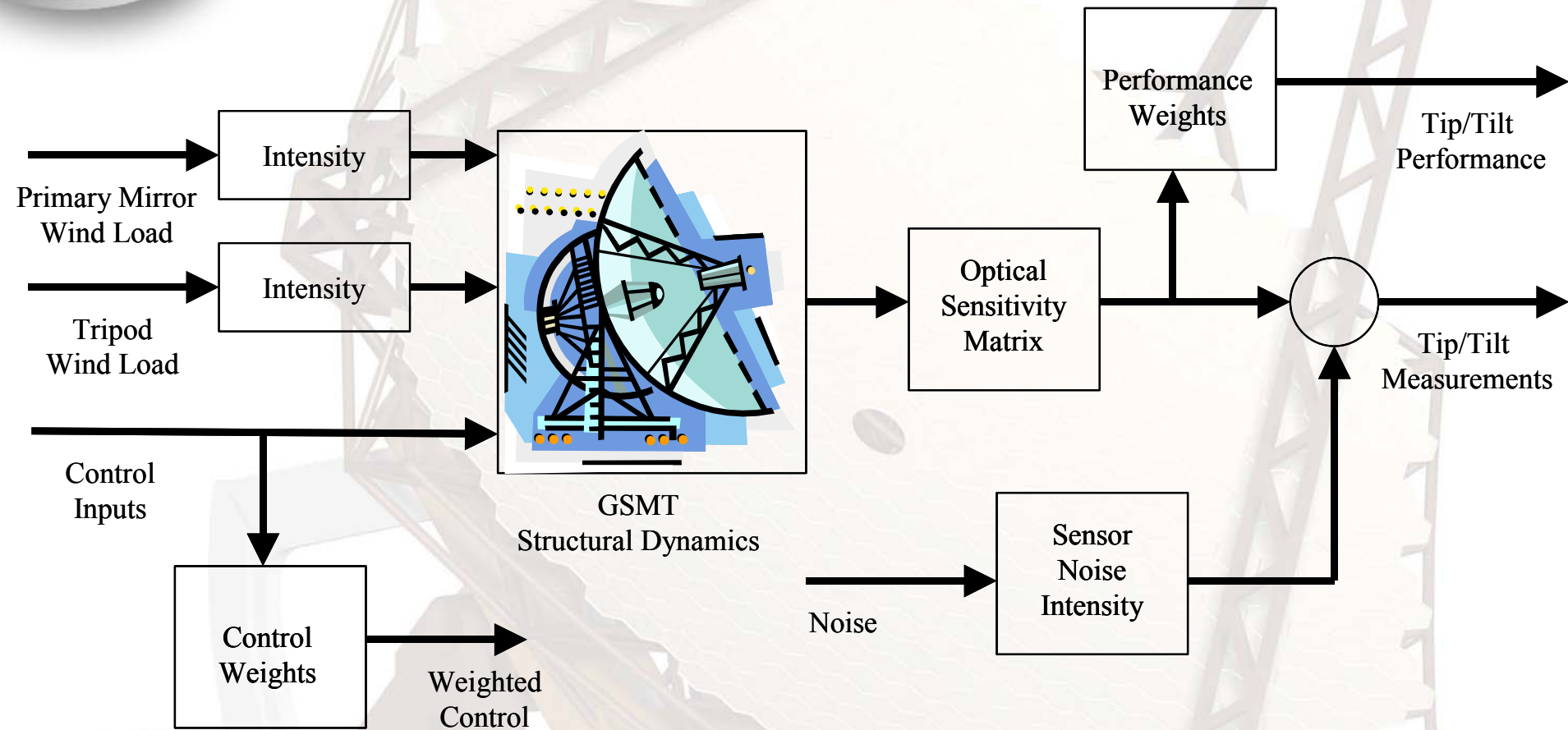
Secondary Mirror Detail

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Secondary Mirror Control

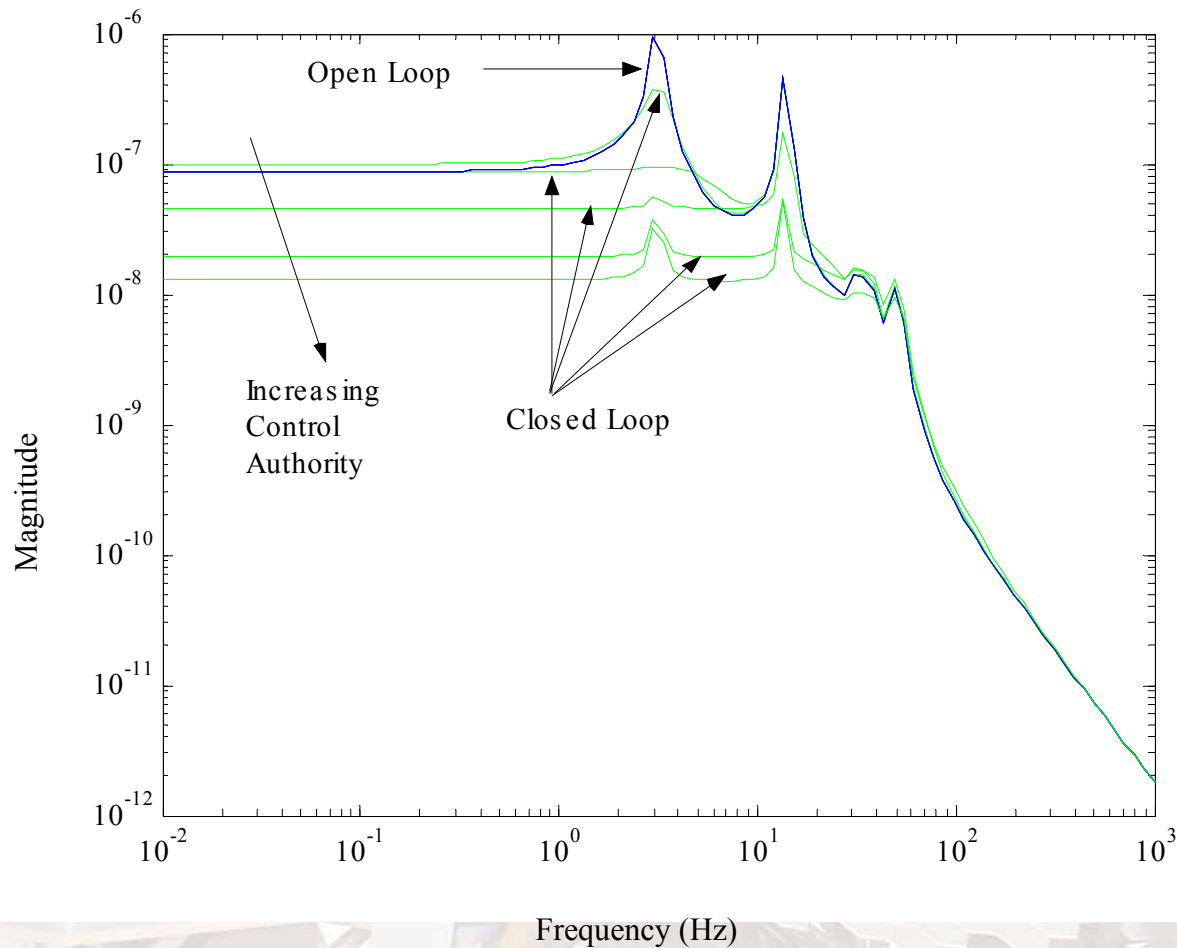
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Control Design Results

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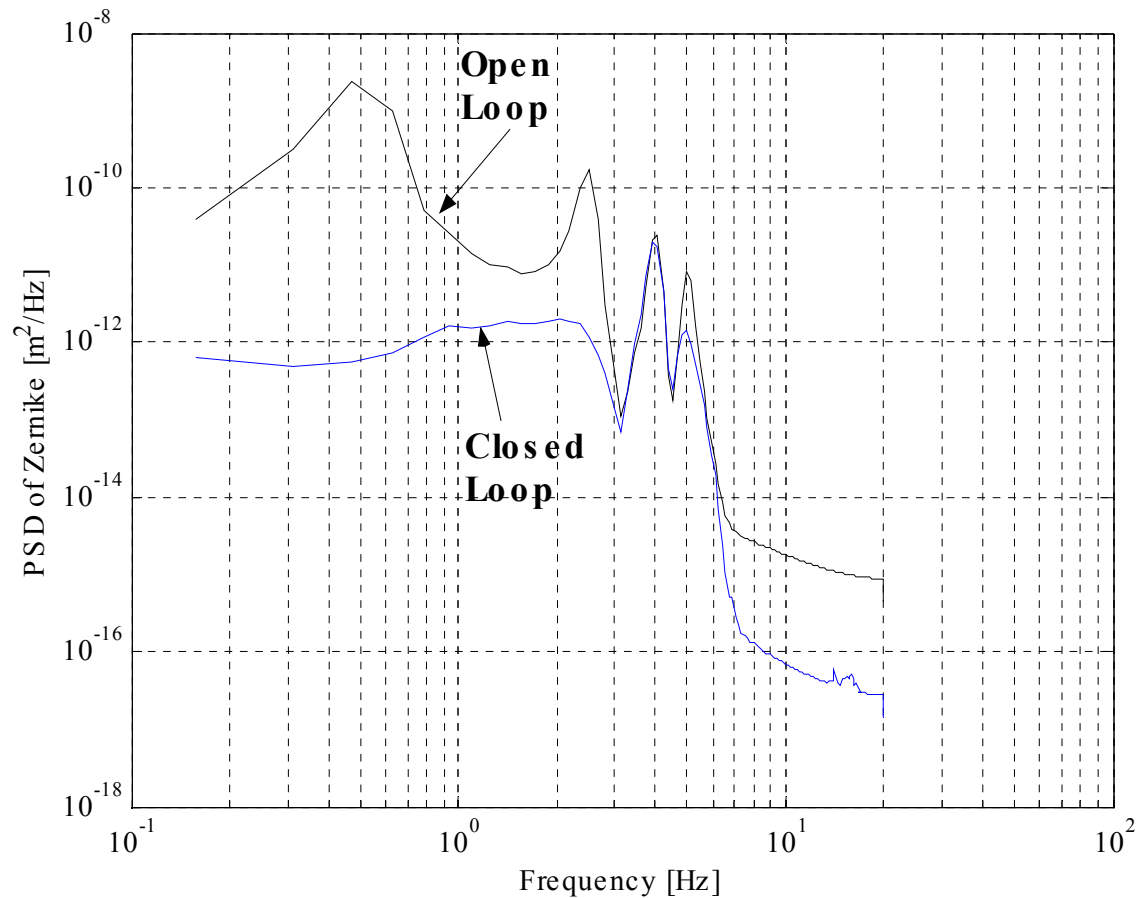
Open and Closed Loop Maximum Singular Values



Control Design Results

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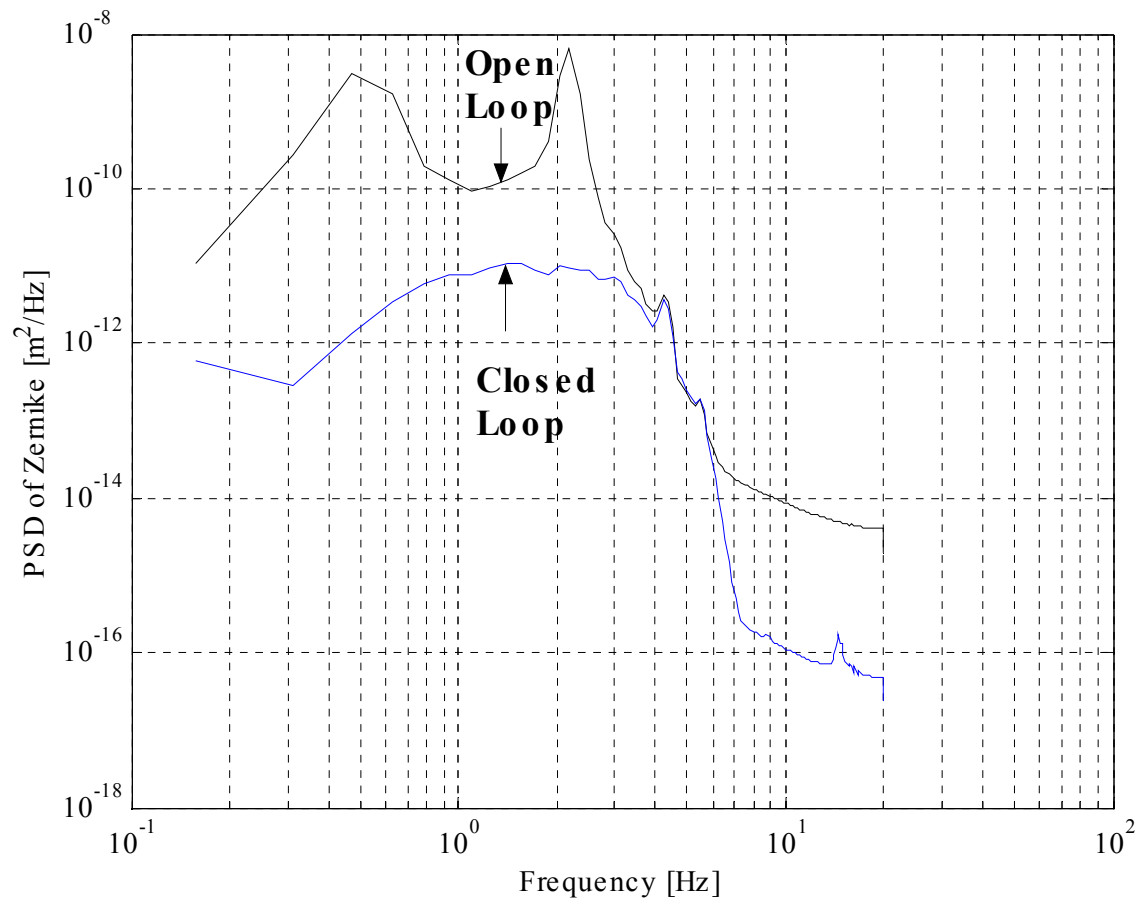
Open and Closed Loop PSD of X-Tip (Total OPD)



Control Design Results

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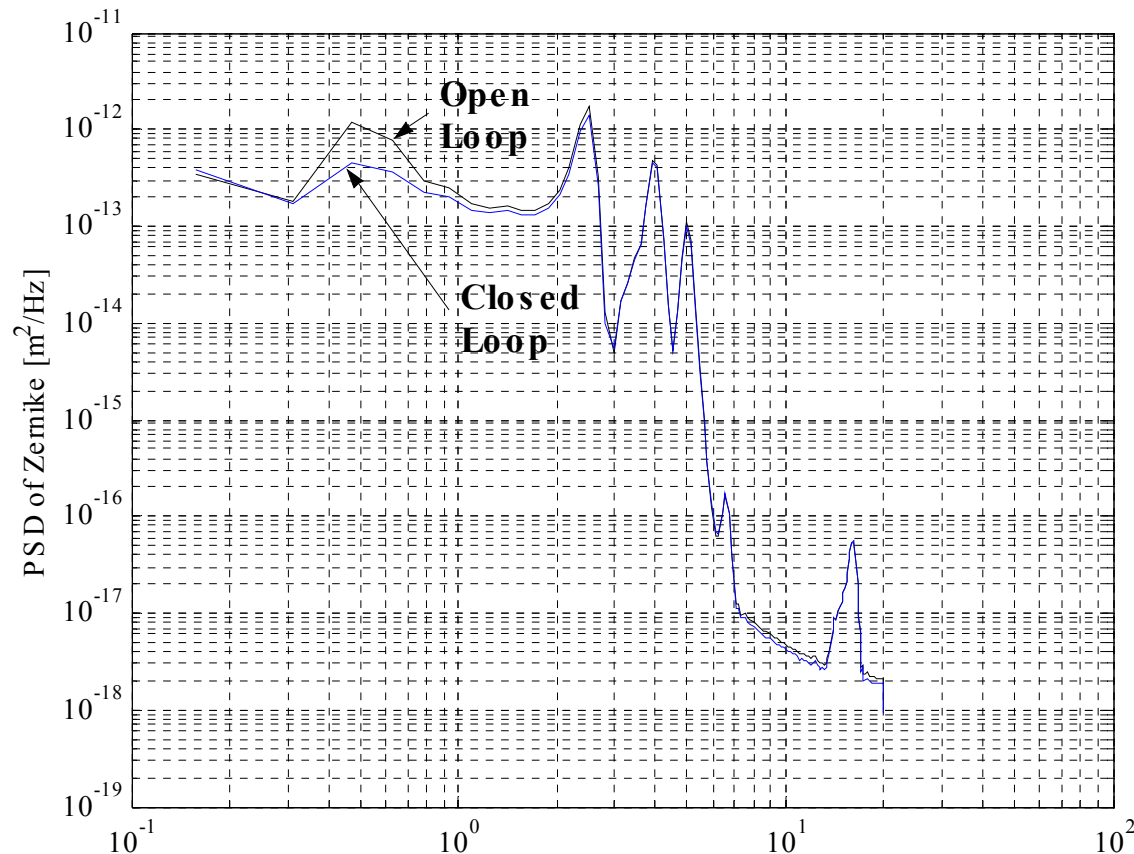
Open and Closed Loop PSD of Y-Tip (Total OPD)



Control Design Results

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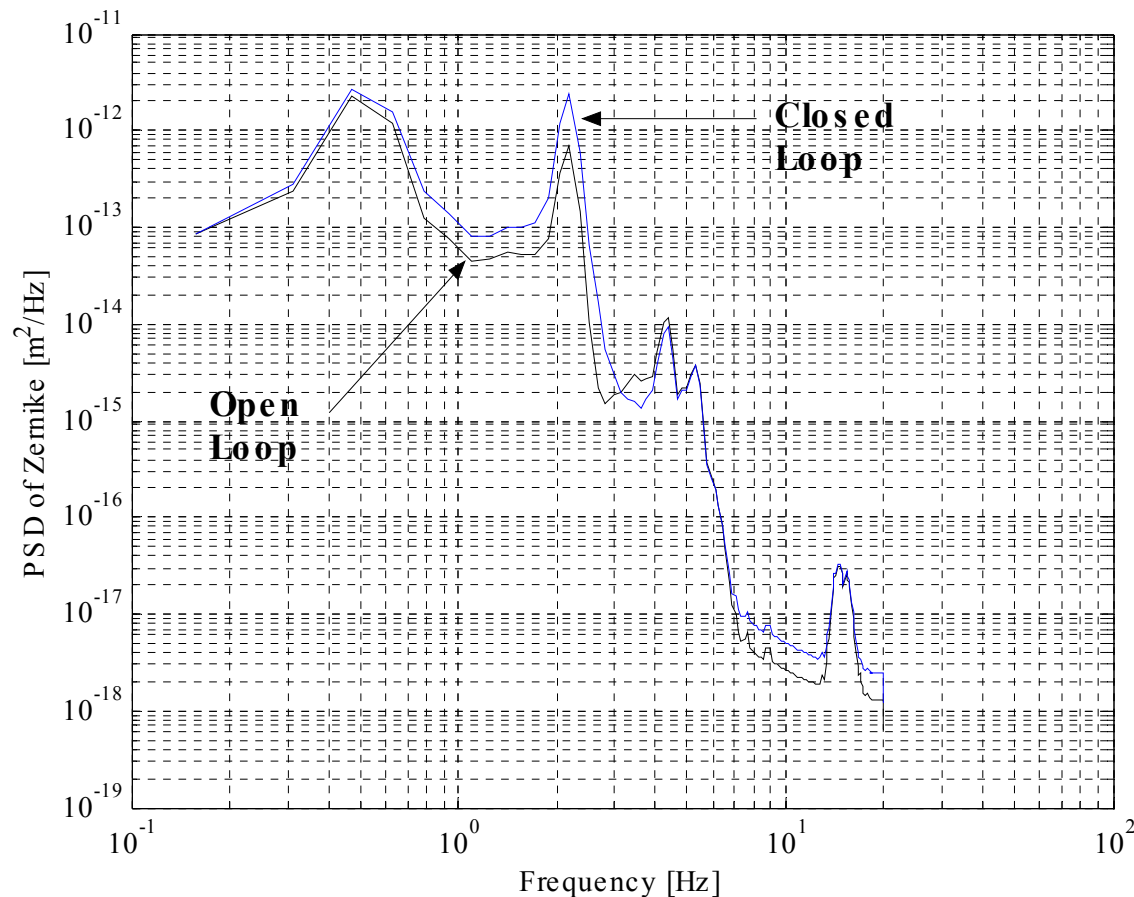
Open and Closed Loop PSD of 0° Coma (Total OPD)



Control Design Results

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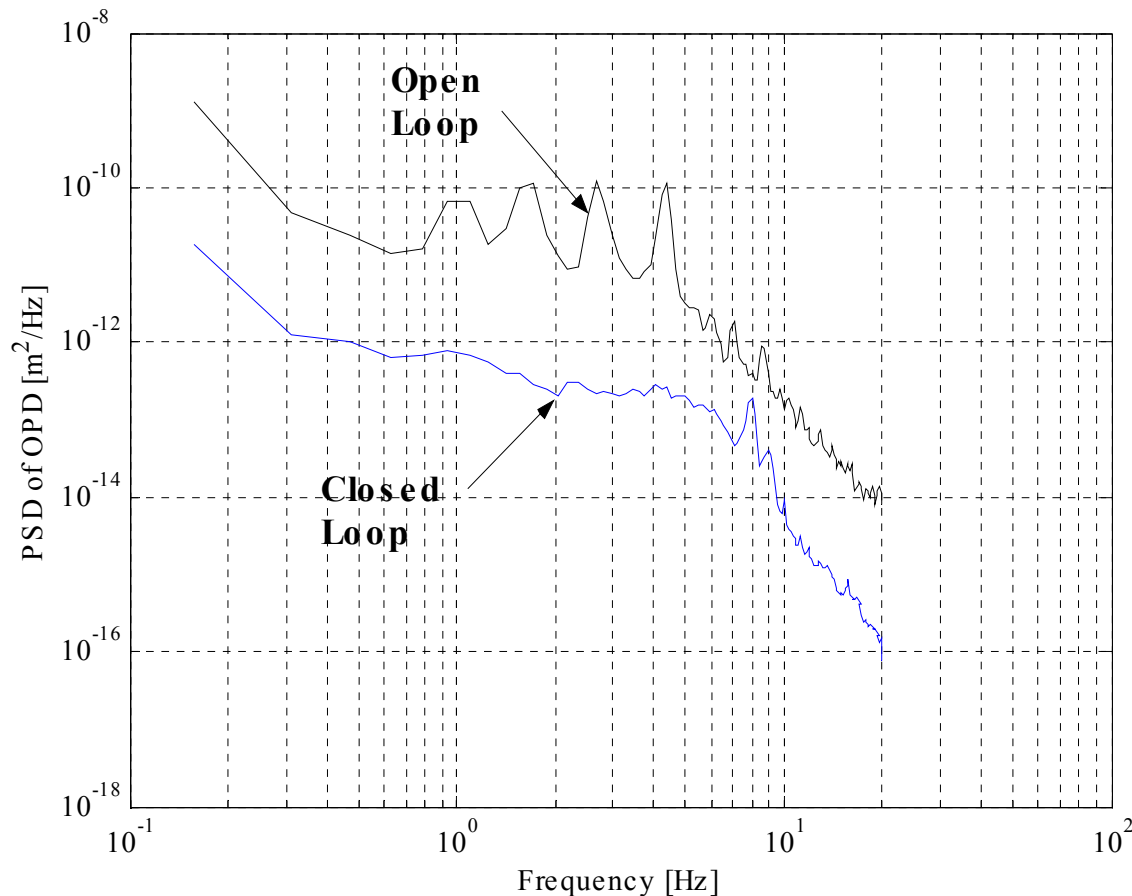
Open and Closed Loop PSD of 90° Coma (Total OPD)



Control Design Results

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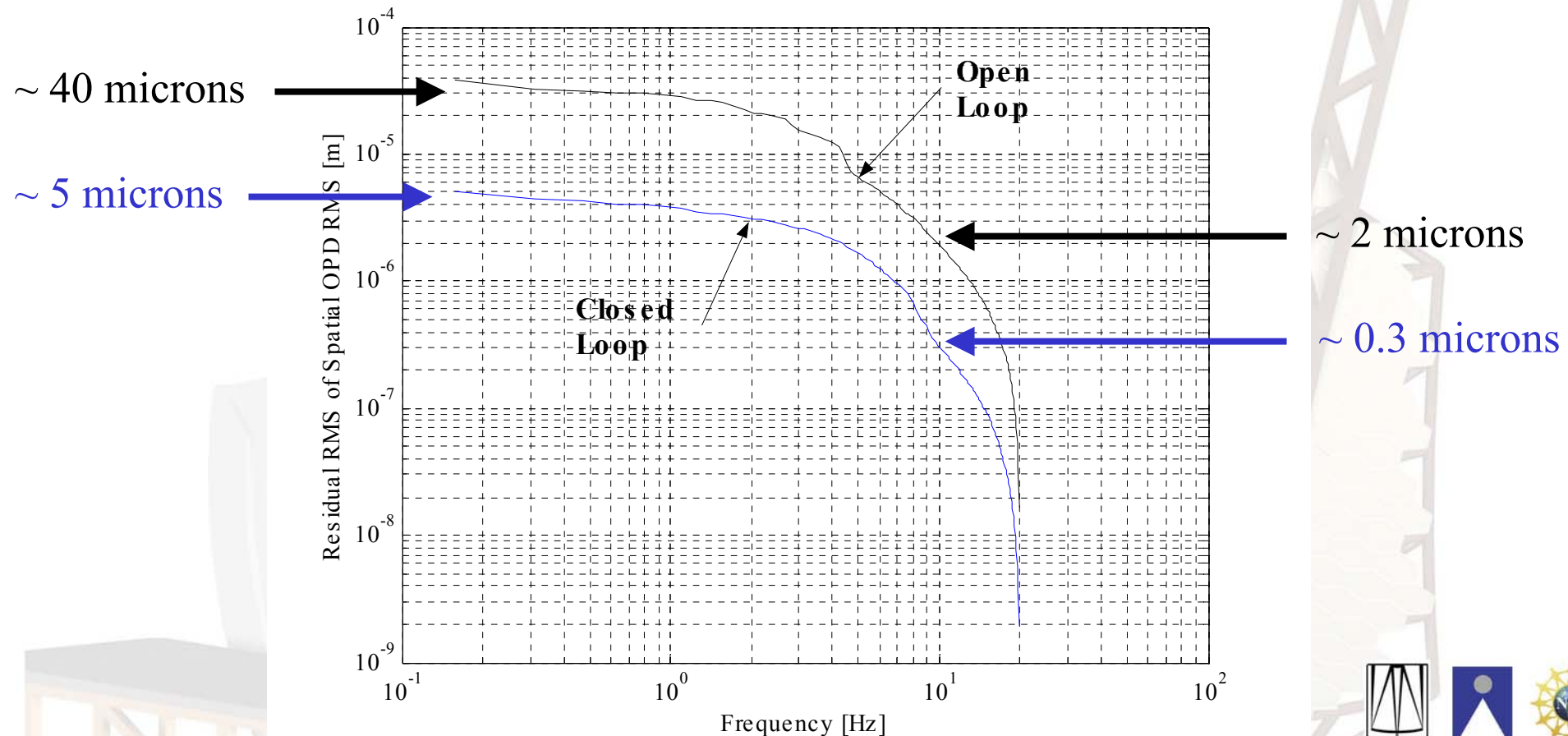
Open and Closed Loop PSD of Spatial RMS of Total OPD



Control Design Results

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Residual RMS of the Spatial RMS of Total OPD



Conclusions

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- **Identified evolution of control challenge to giant telescopes**
- **Investigated feasibility of control architecture applied to rigid secondary support**
- **Demonstrated reduction of image aberrations induced by telescope vibration**
- **Provided motivation and demonstration of utility of modern control method**

